

# Cold Sprayed HEA Coatings

Microstructure and Tribological Behaviour of Cold Spray  
 $\text{AlCoCrFeNi}_{2.1}$  Eutectic High-Entropy Alloy

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32<sup>nd</sup> Cold Spray Club, June 2025, Gallipoli, Italy



# MATERIALS AND PROCESSES

## Areas of expertise

- Polymers and bioproducts
- Advanced polymer composites
- Simulation and numerical modeling
- Powder forming
- Materials for energy technologies
- Thermal spray

## Objectives

- **Develop novel materials & processes**
- **Provide expert services to Canadian industry across many sectors: e.g. automotive, aerospace, defense, medical devices, energy**
- **Support innovation and competitiveness**

# NRC-Thermal Spray Facility and Equipment

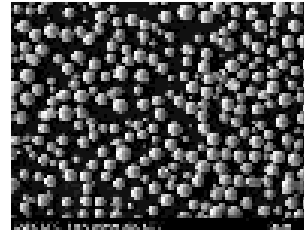


- 5 dedicated robotic spray booths
- 21 commercial spray systems (Plasma, Wire-arc, cold spray, HVOF, Flame)
- Comprehensive process diagnostics, monitoring and numerical simulation capabilities (Industry 4.0)
- Comprehensive thermal spray coating testing and characterization capabilities
- Thermal cycle laser rig and thermal cycle water vapor rig for thermal and environmental barrier coatings

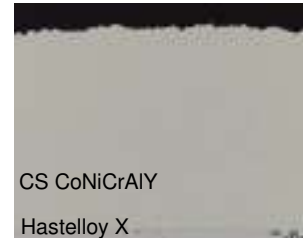
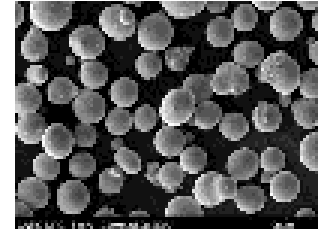
# NRC R&D on Cold Spray of MCrAlYs

- Feedstock: MCrAlX (M=Co, Ni and X= Y, HfSi)
- High-pressure CS: N<sub>2</sub> used as propelling gas
- Effect of powder granulometry, gas temperature / pressure / standoff distance (SOD) / gun traverse speed
- Very well adhered and dense cold-sprayed coatings
- Roughness: 6 to 12um, tunable with powder granulometry
- Porosity: 1 to 2.5% depending on feedstock PSD
- Bond strength:  $> 70 \pm 5$  MPa

'Fine': -22/ +5  $\mu\text{m}$



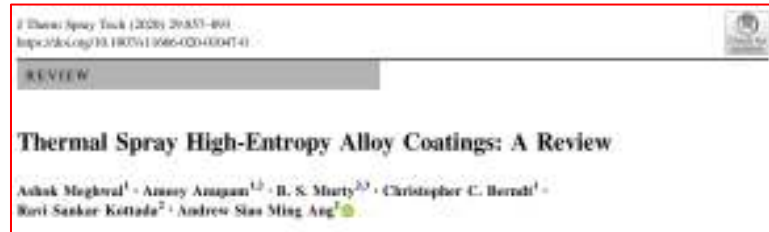
'Coarse': -45/+20  $\mu\text{m}$



# Emerging materials: High Entropy Alloys (HEA)

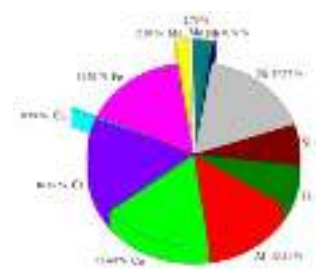
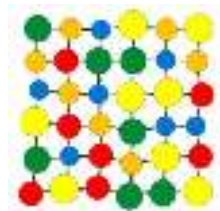
**HEAs: solid solution alloys of five or more elements in equi- or near-equi-atomic ratios**  
(Yeh and Cantor 2004)

*More broadly: alloys containing  $n$  major elements, where  $n$  is between 5 and 13, and the molar ratio of each element is from 5 to 35 at%.*

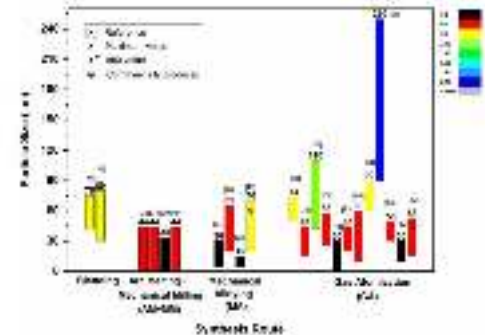


## Reasons for HEA special properties

- High mixing entropy
- Sluggish diffusion
- Lattice distortion
- Cocktail effect



Elements occurrence in HEA used as a feedstock for different TS processes



Synthesis routes reported to construct HEA feedstocks for TS:  
(1) blending, (2) arc melting followed by mechanical milling, (3) mechanical alloying, and (4) gas atomization.

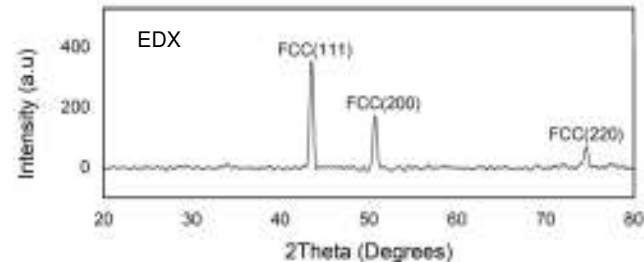
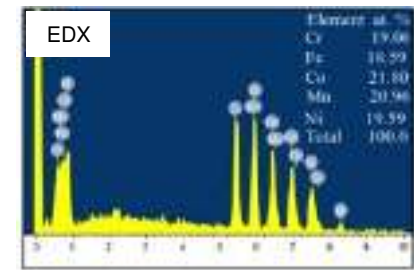
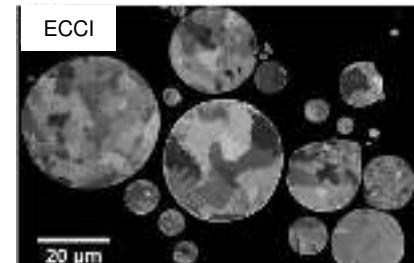
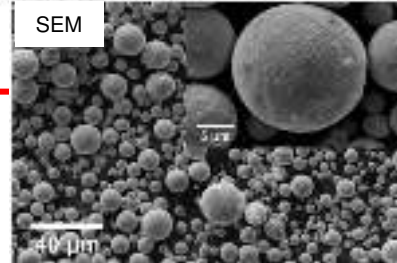


# Cold Spray and Laser-Assisted Cold Spray of CrMnCoFeNi High Entropy Alloy Using Nitrogen as the Propelling Gas

Roghayeh Nikbakht<sup>1</sup> · Cristian V. Cojocaru<sup>2</sup> · Maniyya Aghasibeig<sup>3</sup> ·  
 Éric Irissou<sup>2</sup> · Taek-Soo Kim<sup>4</sup> · Ilyoung Seop Kim<sup>5</sup> · Bertrand Jodoin<sup>1</sup>

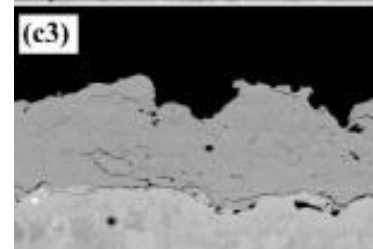
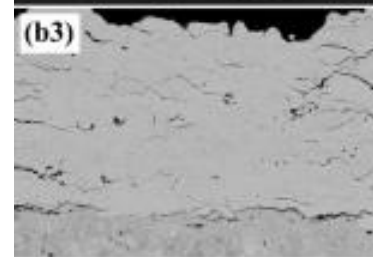
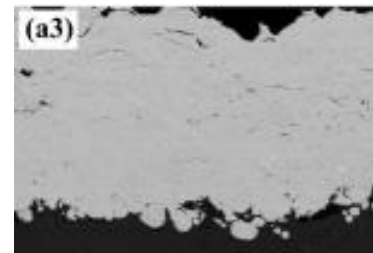
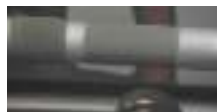
## CrMnCoFeNi: Cantor alloy

- single-phase solid solution
- powder: spherical morphology
- dendritic grain distribution
- PSD: +9.5/-45um,D50=25um
- FCC crystal structure



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HEA  
 CrMnCoFeNi  
 coatings  
 on different  
 substrates

Al6061

steel

Hastelloy X

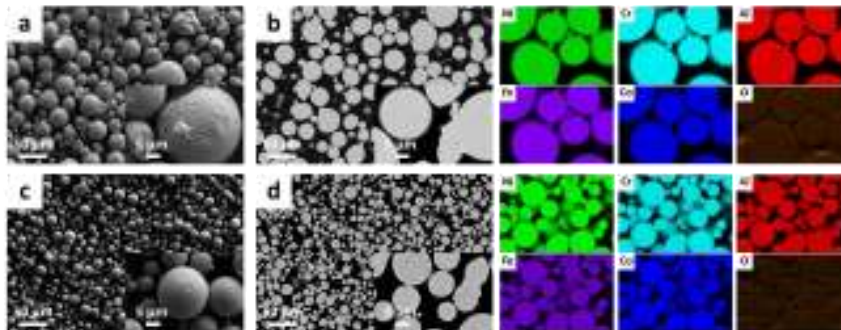
| Substrates              | Al6061          | Mild steel      | Hastelloy X     |
|-------------------------|-----------------|-----------------|-----------------|
| $R_a$ ( $\mu\text{m}$ ) | $4.68 \pm 0.16$ | $3.70 \pm 0.19$ | $2.72 \pm 0.22$ |
| Hardness (HV) at 300gf  | $104 \pm 1.9$   | $204 \pm 2.36$  | $236 \pm 0.85$  |

# HEAs vs. MCrAlYs

## HEA Chemistries Explored

| Alloy                            | Co    | Ni        | Cr   | Al      | Y   | Fe |
|----------------------------------|-------|-----------|------|---------|-----|----|
| CoNiCrAlY (wt.%)                 | 38    | 32        | 21   | 8.5     | 0.5 | -  |
| NiCoCrAlY (wt.%)                 | 21-22 | 46.5-49.5 | 18   | 11-13   | 0.5 | -  |
| AlCoCrFeNi (at.%)                | 20    | 20        | 20   | 20      | -   | 20 |
| AlCoCrFeNi (wt.%)                | 23.5  | 23        | 20.5 | 10.5-11 | -   | 22 |
| AlCoCrFeNi <sub>2.1</sub> (at.%) | 17    | 35        | 16   | 16      | -   | 16 |
| AlCoCrFeNi <sub>2.1</sub> (wt.%) | 19    | 39.5      | 16   | 8.5     | -   | 17 |

(a) and (b) 3D and cross-section SEM of AlCoCrFeNi equiatomic powder (+15/-53um).



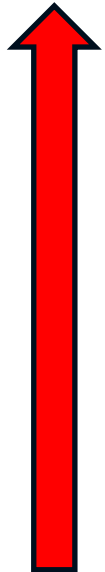
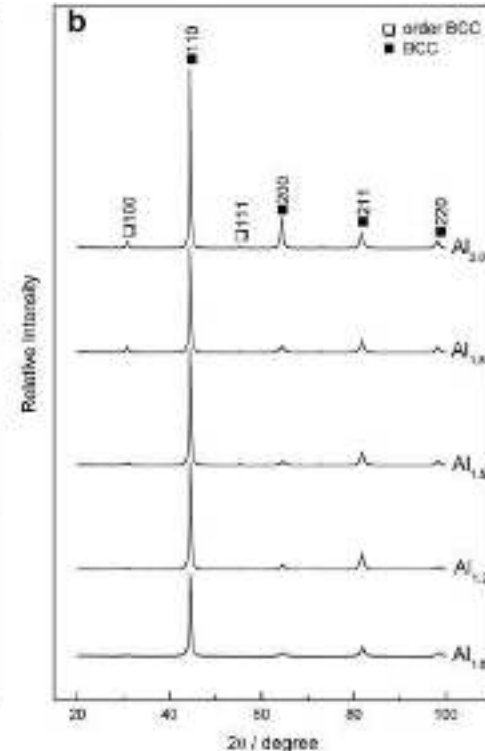
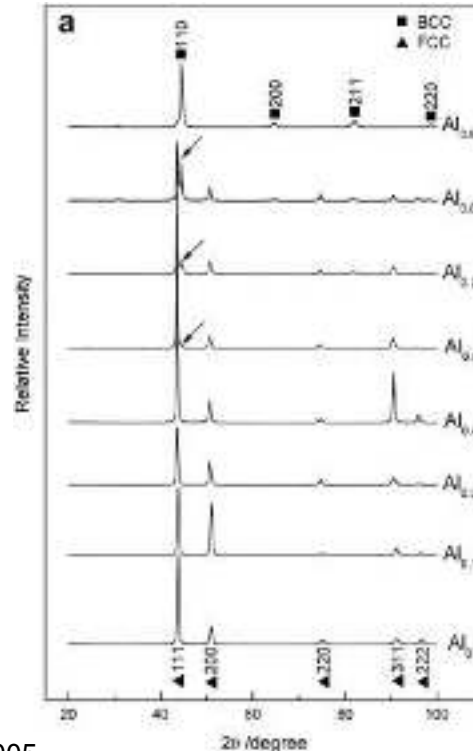
(c) and (d) 3D and cross-section SEM of AlCoCrFeNi<sub>2.1</sub> eutectic powder (+5/-25um).

EDX mapping of both equiatomic and eutectic HEA compositions



# The **Al**CoCrFe**Ni**<sub>2.1</sub> System

- **Al** is the BCC stabilizer; addition of **Al** promotes the formation of **NiAl** BCC/B2
- **Ni** is the FCC stabilizer, with ~2.1 mole ratio of Ni, we achieve the eutectic composition

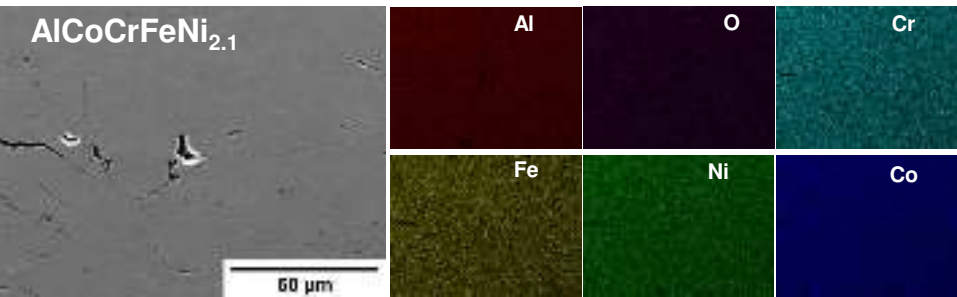


Increasing  
Al  
content

# Deposition, microstructure and hardness of $\text{AlCoCrFeNi}_{2.1}$ entropic high entropy alloy coatings by cold spray, HVOF, and plasma spray

Jingjie Wei<sup>a</sup>, Cristian Cajocanu<sup>a</sup>, Maniya Aghasheibi<sup>b</sup>, Chenwei Shan<sup>a</sup>, Zehua Li<sup>a</sup>,  
Jialun Zhang<sup>a</sup>, Eric Lissou<sup>b</sup>, Yu Zou<sup>a</sup>

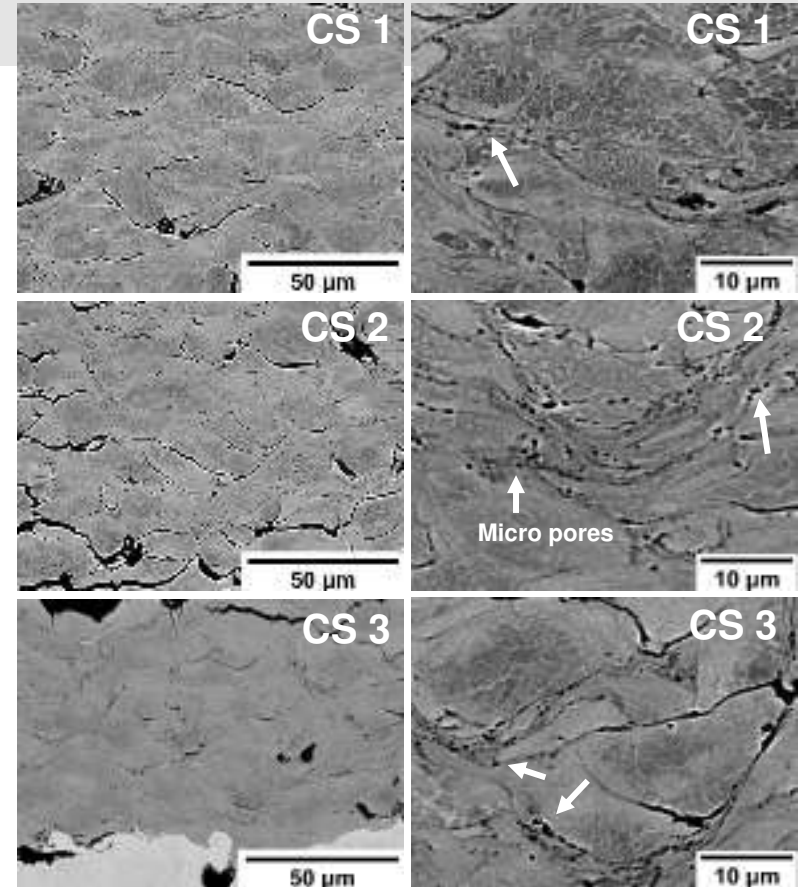
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<sup>b</sup> *National Research Council Canada, Boulder CO, CO 80501, Canada*



EDS cross-section mapping

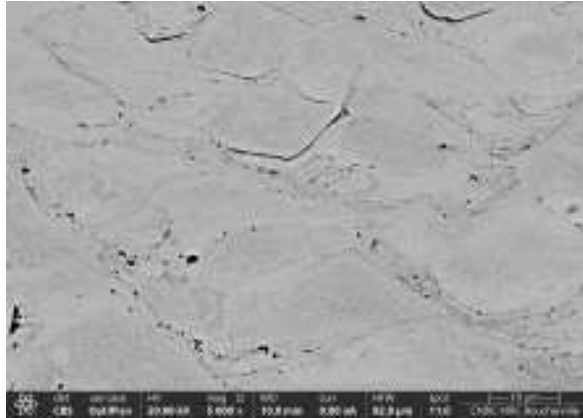
- No signs of elemental segregation or microstructure changes
- Higher traverse speed increases micropores at particle interfaces, potentially leading to weaker bonding

## SEM BSE of coating cross-section

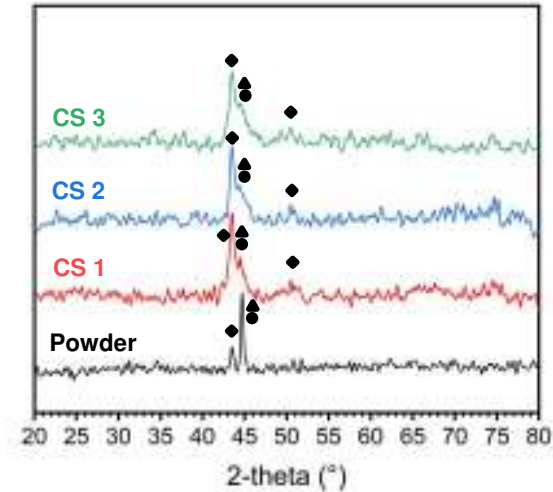


# AlCoCrFeNi<sub>2.1</sub> Coatings: Phase Transformations

Cold Spray Giken PCs100



Pgas:7.5MPa; 950°C; SOD 50mm; vgun;200mm/s

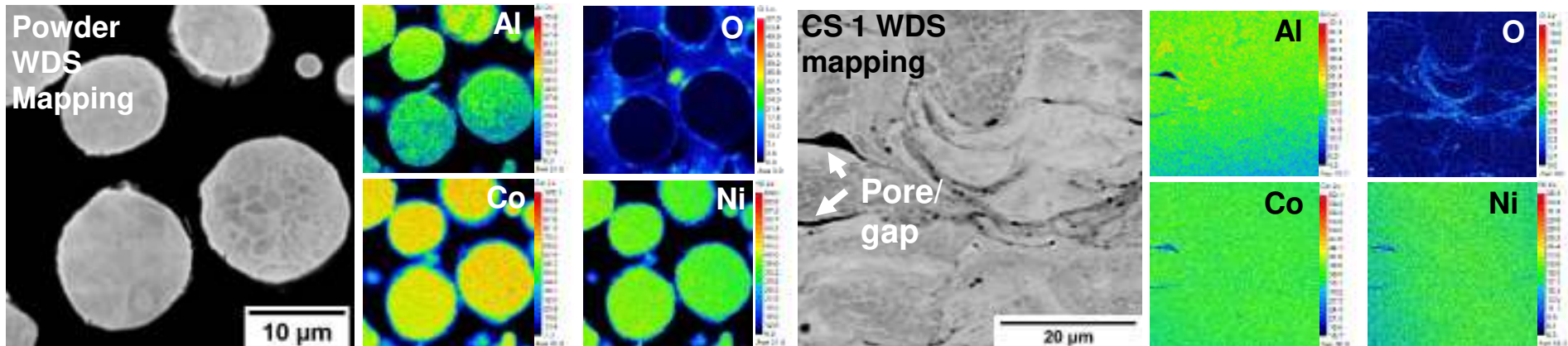


- Cold spray (high strain/strain rate) favours preservation of FCC CoCrFeNi rich phase
- Peak broadening + low signal-to-noise ratio indicate high residual strain and dislocation density



# Cold Spray: Preservation of Microstructure

WDS: Wavelength Dispersive Spectroscopy

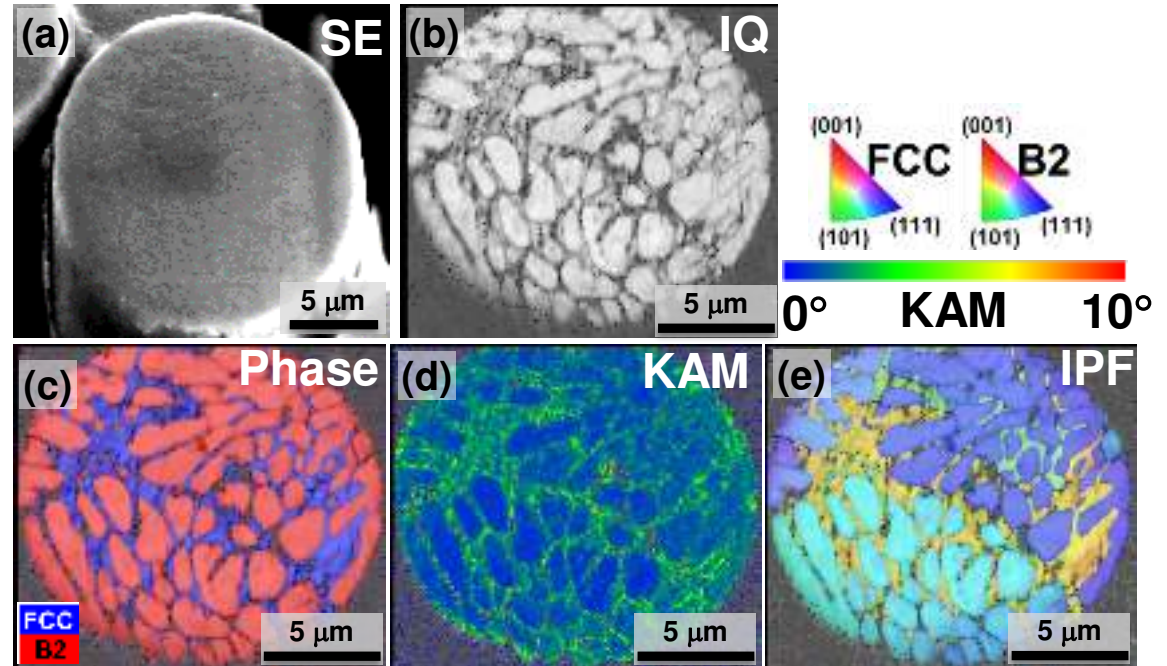


- Comparison with feedstock powder indicate successful preservation of microstructure
- Thin layer of oxide at particle interfaces
- No signs of significant elemental segregation/diffusion in lamellar microstructure



# AlCoCrFeNi2.1 Eutectic High Entropy Alloy Powder Features via EBSD Analysis

- Mostly spherical particles with a size range of  $\sim 5 - 30 \mu\text{m}$ .
- FCC + B2 dual-phase powders with eutectic B2 embedded in FCC matrix.
- Average volume fraction of phases:
  - FCC = 35%
  - B2 = 65%
- Each powder exhibits similar orientation profile for B2 phases, whereas FCC orientation changes.

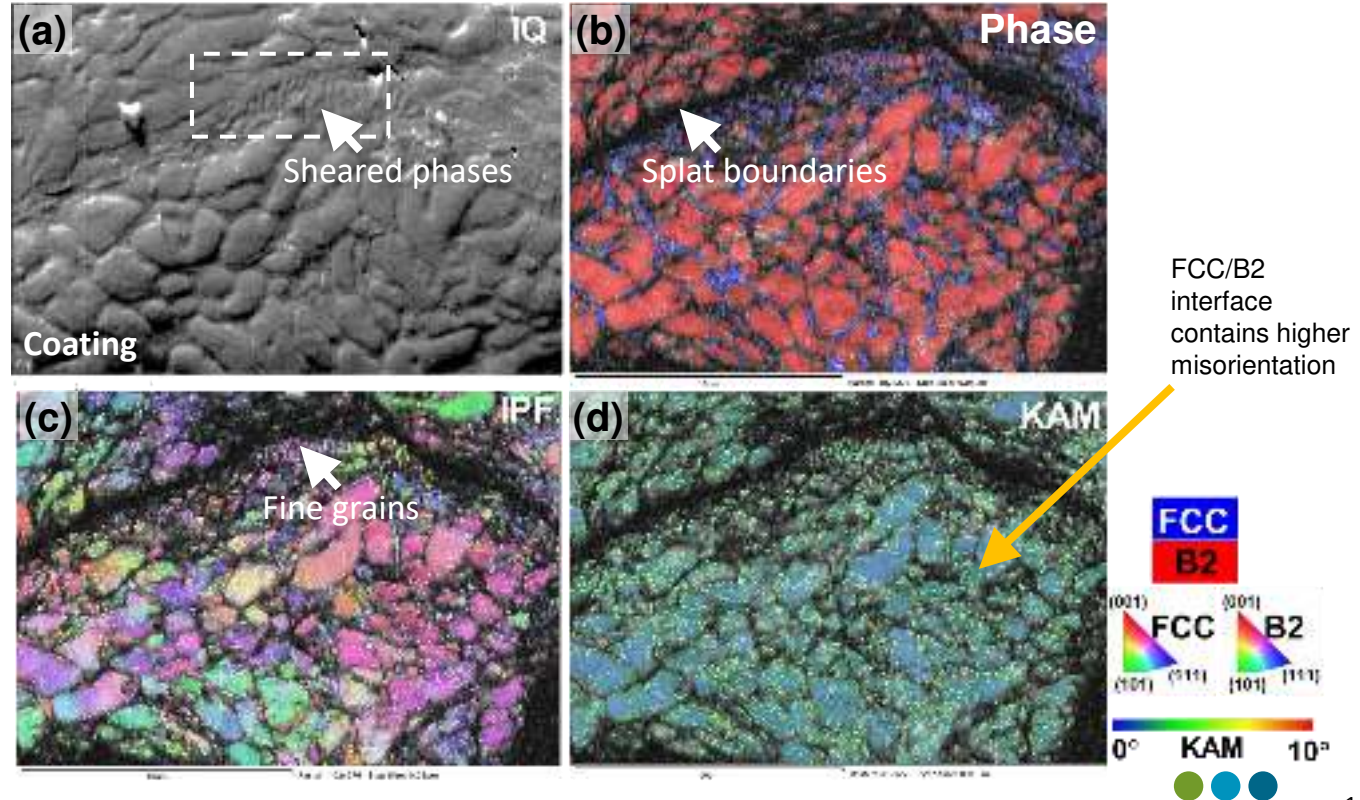


Collaboration with Prof. Yu Zou, Dept. of Mat. Science, Univ. of Toronto



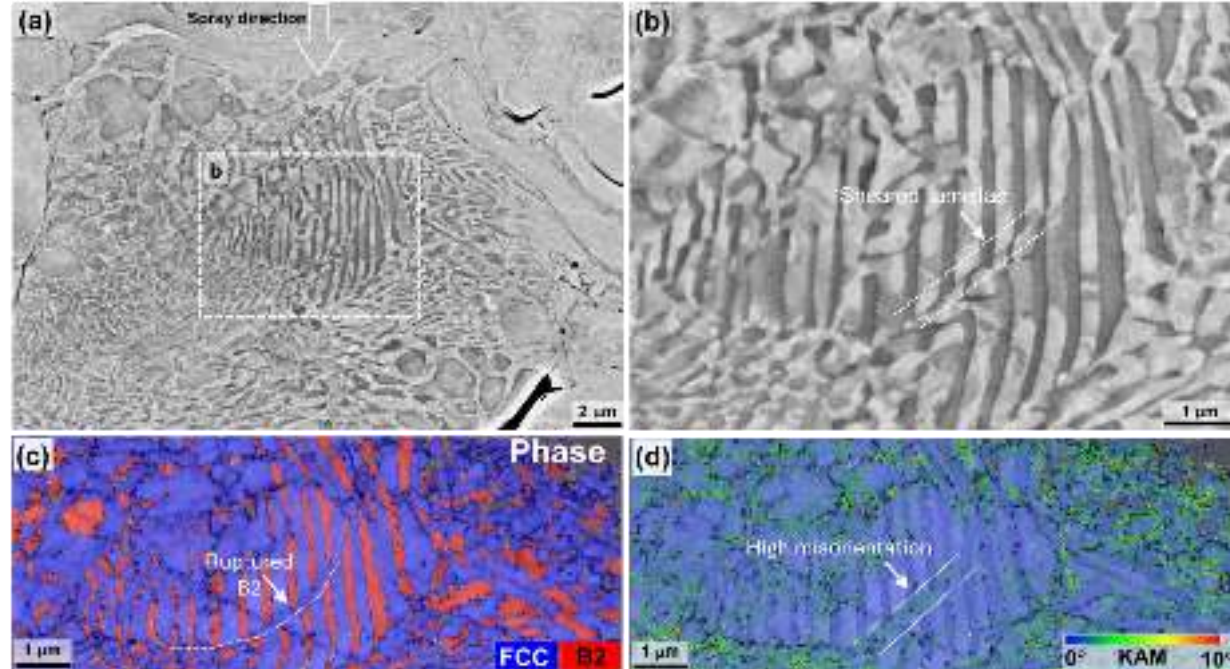
# Deformation features of the cold sprayed EHEA coating via EBSD Analysis

- Closer to the particle boundary higher FCC content is observed.
- FCC inter-dendritic regions are dynamically recrystallized.
- B2 grains prevail with less deformation and not much lattice rotations
- Further, HR-TKD and TEM analysis will be performed to understand inter-particle boundary deformation mechanisms.



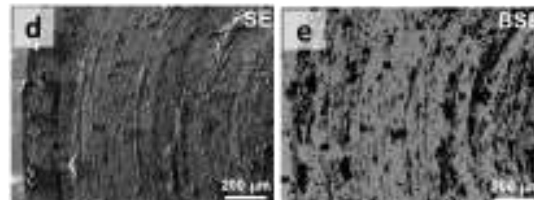
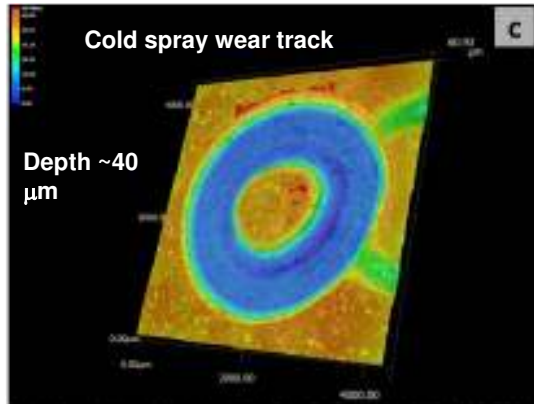
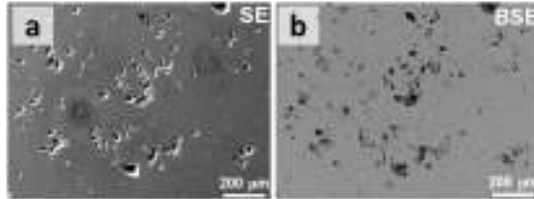
# Deformation features of the cold sprayed EHEA coating

- To study why the lamellar eutectic structure is prone to cracking, internal eutectic structure are analyzed in the coating.
- Cracking initiates from shearing of the thin FCC and B2 lamellae.
- Network FCC and dendritic B2 have higher volume to accommodate severe plastic deformation.
- Lamellar FCC and B2 show shear at ballistic ( $\sim 10^9 \text{ s}^{-1}$ ) impact strain rates and tend fracture early.
- More misorientation can be observed within the sheared region owing to severe strain localization.



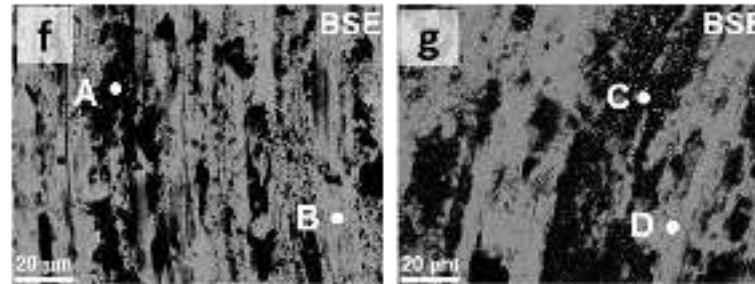
# Cold Spray AlCoCrFeNi<sub>2.1</sub>

## *Wear behavior*



Al<sub>2</sub>O<sub>3</sub> balls (1/4 in. in diam.) under a load of 10 N for 30 min. at 100 RPM and with 1 mm track radius.

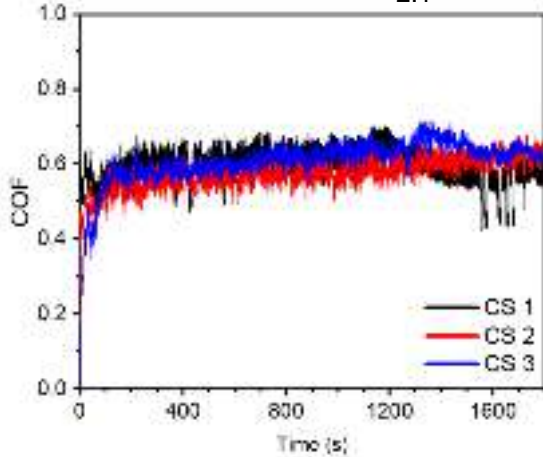
- Initial (polished) surface before wear tests shows pores; this could increase the CoF and provide higher resistance to wear.
- Tracks show debris accumulation → the cause of peaks in CoF plot.
- Dark oxide mostly (Fe, Ni)O patches in BSE limit further wear.



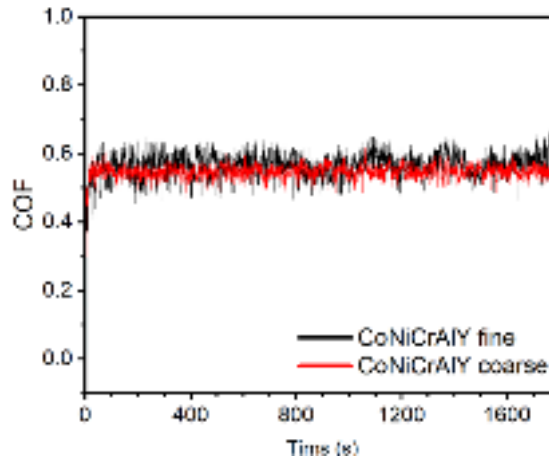
| Points | Al<br>(wt.%) | Co<br>(wt.%) | Cr<br>(wt.%) | Fe<br>(wt.%) | Ni<br>(wt.%) | O<br>(wt.%) |
|--------|--------------|--------------|--------------|--------------|--------------|-------------|
| A      | 10.6         | 13.9         | 18.7         | 23.5         | 19.5         | 13.8        |
| B      | 9.1          | 18.2         | 17.2         | 17.3         | 35.9         | 2.4         |
| C      | 18.2         | 10.9         | 9.5          | 15.1         | 21.7         | 24.5        |
| D      | 13.1         | 12.5         | 13.5         | 17.7         | 42.9         | 0.3         |

# Wear Performance: Cold Spray EHEA vs. CoNiCrAlY

Cold Spray  
AlCoCrFeNi<sub>2.1</sub>



Cold Spray  
CoNiCrAlY



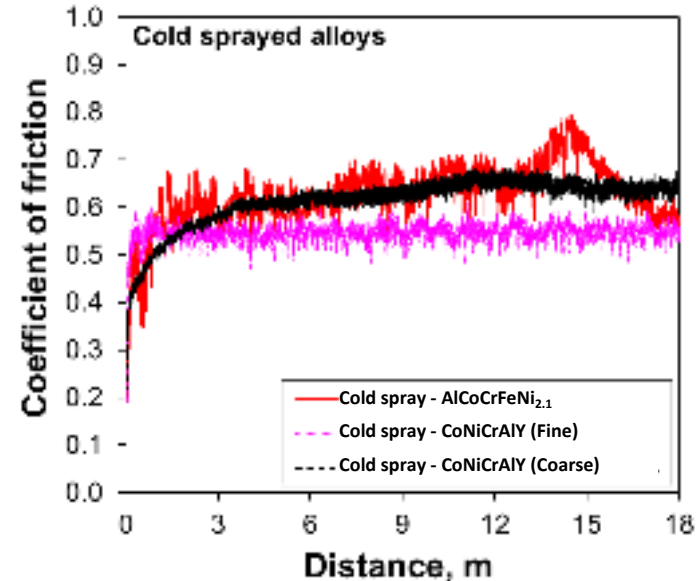
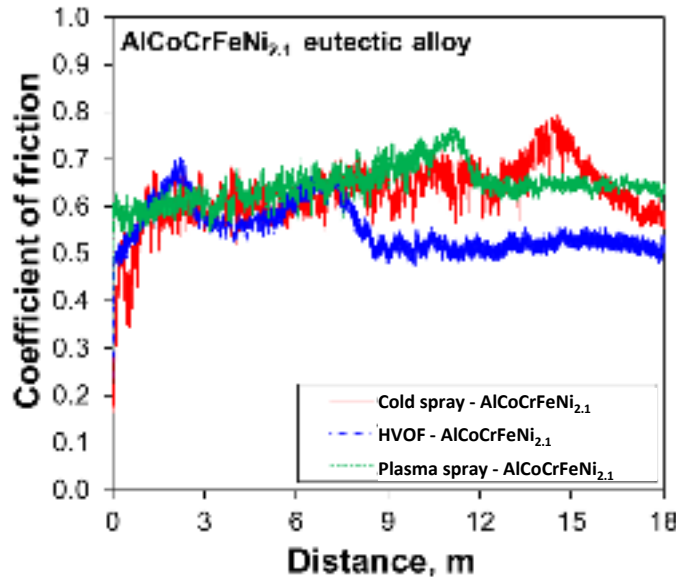
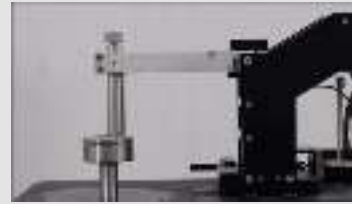
Pin-on-disk wear test:  
Room Temperature  
10N, 1mm radius, 100 RPM, 30 mins

- Cold sprayed EHEA and CoNiCrAlY coatings show similar COF
- Analysis of wear rates is necessary to draw conclusions

| material         | Pgas<br>[MPa] | Tgas<br>[°C] | SOD<br>[mm] | Vgun<br>[mm/s] |
|------------------|---------------|--------------|-------------|----------------|
| CoNiCrAlY fine   | 7.5           | 950          | 50          | 100            |
| CoNiCrAlY coarse | 7.5           | 950          | 50          | 100            |



# Coefficient of friction

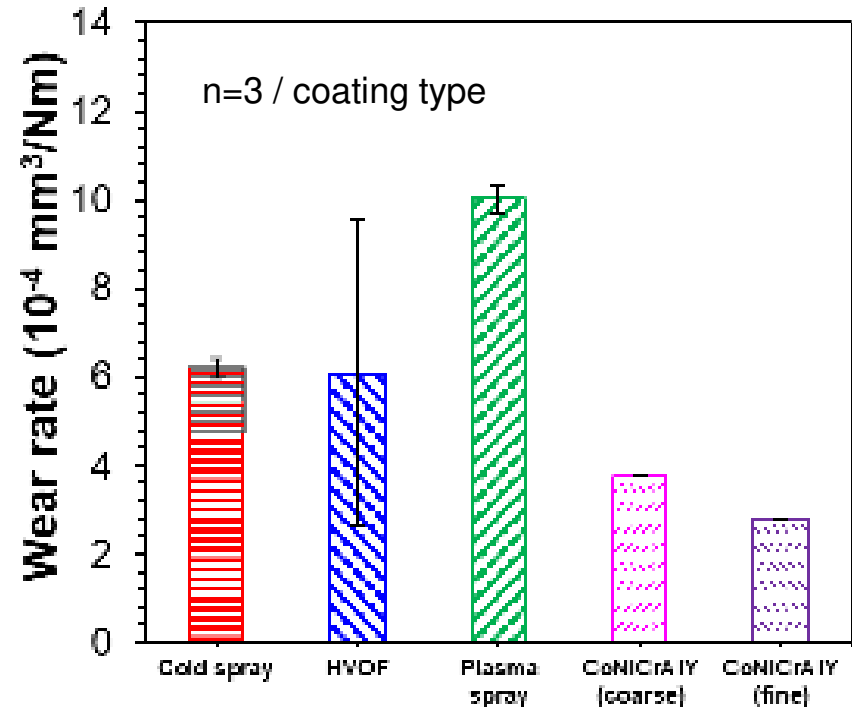


- All EHEA coatings show transition in the CoF at different stages:
  - Effect of the presence of oxides and their distribution.
  - In a first step, agglomeration of worn oxide particles increase CoF.
  - Accumulation of oxides agglomerates lead to formation of an oxide layer → decrease CoF.



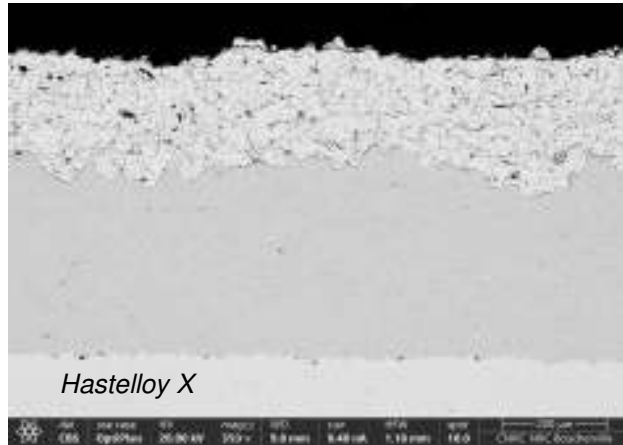
# Wear rate: a comparison CS vs. HVOF vs. APS

- ❑ CS and APS coatings show stable wear rates compared with HVOF coating.
- ❑ HVOFs with lower average rate of wear could arise from the interplay of:
  - Formation of oxide layer lubrication at different time intervals
  - Accumulation of lubricating oxides leading to low wear rate
- ❑ CoNiCrAlYs with Yttrium doping has higher chances of forming tribo-oxide layer → Lower wear rate.



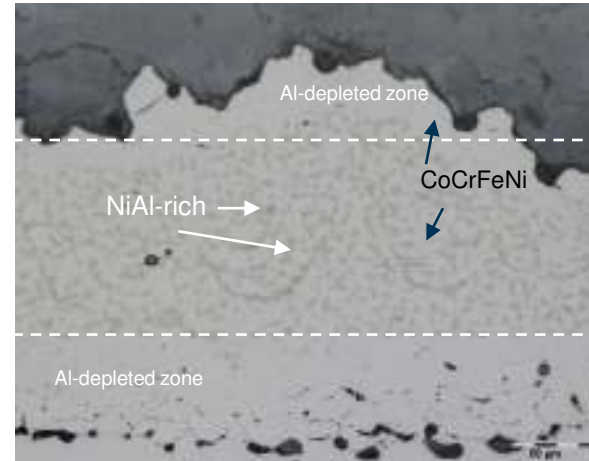
# Cold Spray AlCoCrFeNi<sub>2.1</sub> as Bond Coat

As-sprayed TBC



Bond Coat: Cold sprayed AlCoCrFeNi<sub>2.1</sub>

Top Coat: APS 8wt% YSZ



Furnace cycling testing: sample after  
125 cycles @ 1150°C in air

# Summary & Future Work

- Successful deposition of dense AlCoCrFeNi<sub>2.1</sub> EHEA coatings by cold spray
- Cold spray produces EHEA coatings with high hardness and minimal oxidation
- Microstructure is preserved yet phase transformation occurs due to rearrangement of the metastable BCC/B2 structure
- EHEA coatings show transition in the coefficient of friction (CoF) at different stages
- The accumulation of oxides agglomerates during wear tests lead to formation of an oxide layer and decrease CoF
- Continue wear behaviour study using both room temperature and high temperature (1000°C) setup
- Effects of annealing/high temperature testing on microstructure of deposited coatings
- Observe the development of oxide layer (i.e. thermally grown oxides in TBCs)

# Thank you!

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